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Tucson Electric Power Company

P.O. Box 711, Tucson, AZ 85702 One South Church Avenue, Suite 200, Tucson, Arizona 85701

January 31, 2008 Ū Arizona Corporation Commission 1200 West Washington Street See. 1 Phoenix, AZ 85007

Docket No. E-00000D-07-0376 Re:

Docket Control:

Docket Control

Enclosed please find an original and thirteen copies of Tucson Electric Power Company's ("TEP") "Ten-Year Plans" pursuant to Title 40, Chapter 2, Article 6.2, "Power Plant and Transmission Line Siting Committee", of the Arizona Revised Statutes. TEP's RMR study, per Staff request, is being provided to Commission Staff directly.

Enclosed is an additional copy of the filing that the Company requests you date-stamp and return in the self-addressed, stamped envelope for our files.

Sincerely,

issicatsupe

Jessica Bryne **Regulatory Services**

Arizona Corporation Commission DOCKETED JAN 31 2008 DOCKETED BY

Ernest Johnson, ACC cc: Prem Bahl. ACC Ed Beck, TEP Compliance, ACC (cover letter only)



A UniSource Energy Company

TUCSON ELECTRIC POWER COMPANY TEN YEAR PLAN FOR YEARS 2008-2017

SUBMITTED TO THE ARIZONA CORPORATION COMMISSION JANUARY 2008

DOCKET NO:

E-00000D-07-0376

- 1 -

CONTENTS

INTRODUCTION	3
PLANNED TRANSMISSION FACILITIES DESCRIPTIONS	8
ELIV FACUTTIES	8
Interconnection of Westwing – South 345 kV with future Hassyampa – Pinal West 500 kV line via new Pinal W	Vest
500/345 kV Substation	
Pinal South Substation to Tortolita Substation	9
Tortolita Substation to Vail Substation (through North Loop and East Loop Substations)	10
Tortolita Substation to Winchester Substation	11
Winchester Substation to Vail Substation -2^{nd} circuit	12
Vail Substation to South Substation – 2 nd circuit	
Springerville Substation to Greenlee Substation - 2 nd circuit	14
Tortolita Substation to South Substation	15
Westwing Substation to South Substation – 2 nd circuit	16
TEP-Unisource Energy Services 345 kV Interconnection LineSouth Substation to future Gateway Substation	(2 ckts.) 17
Gateway Substation to Comision Federal de Electricidad (CFE) (2 ckts.)	18
HV FACILITIES	19
Irvington Substation to East Loop Substation (through 22nd Street Substation)	19
Vail Substation to East Loop Substation (through Houghton Loop Switching Station*, Spanish Trail and Robe	rts
Substations), tapping the Roberts-East Loop line for new Harrison substation	
East Loop Substation to Northeast Substation (through Snyder Substation)	
Loop existing West Ina Substation to Tucson Station line through Del Cerro (formerly Sweetwater) Substation	n 22
Loop existing Vail Substation to East Loop Substation line through future Pantano and Los Reales Substation.	s 23
Extend 138-kV line from Midvale Substation through future Spencer Switchyard to future San Joaquin Substa	tion 24
South Substation to Duval CLEAR Switchyard (formerly Cyprus Sierrita Extension Switchyard) through future	e Canoa
Ranch (formerly Desert Hills) Substation and Green Valley Substation	
Rancho Vistoso Substation to future Catalina Substation	
Loop existing Irvington Station to Vail Substation #2 line through future University of Arizona Tech Park Sub-	station2 /
Tortolita Substation – Rillito Substation 138 kV	
Tortolita Substation – North Loop Substation, North Loop Substation – Rancho Vistoso Substation and Tortol	lita —
Rancho Vistoso 138 kV corridor expansion and reconfiguration	
Vail Substation – SS NO27 Substation- Cienega Substation – SS NO20 Substation- Spanish Trail Substation 1	38 kV31
New Cienega Substation – Mountain View Substation 138 kV Circuit and Vail Substation – Fort Huachuca To	xp for
Mountain View Substation	
Northeast – Snyder 138 kV – tap for Craycroft-Barril substation	
Irvington – Tucson 138 kV – tap for Kino Substation	
Tortolita Substation – Marana Substation – North Loop Substation 138 kV and Marana Substation – SS NO1	
Substation -North Loop Substation 138 kV	
North Loop Substation - Rancho Vistoso Substation 138kV tap for new Naranja Substation	
DeMoss Petrie Substation – Tucson Substation 138 kV	
Northeast 138 kV Static Var Compensator (SVC)	
North Loop Substation – SS NO4 Substation – DeMoss Petrie Substation 138kV	
Midvale Substation – SS NO22 Substation – South Substation 138kV	
Irvington Substation – Corona Substation –Swan Southlands Substation – SS NO26 Substation – South Substation – 138kV	ation 43
La Canada Substation – Orange Grove Substation– Rillito Substation 138kV	45
Orange Grove Substation-SS NO6 Substation 138kV	
South Substation – Hartt Substation– Green Valley Substation 138kV	
Hartt Substation–SS NO29 Substation 138kV	
Tucson Substation-Downtown Substation 138kV	
DeMoss Petrie Substation – SS NO14 Substation – Northeast Substation 138kV	
Vail Substation – SS NO17 Substation – Irvington Substation 138kV	
APPENDIX A – STATIC VAR COMPENSATOR VOLTAGE STABILITY STUDIES	52

INTRODUCTION

EHV Transmission System

Tucson Electric Power Company (TEP) is a member of the WestConnect Planning Area and the Southwest Area Transmission Planning Group (SWAT). TEP participates in various SWAT subcommittees including: SWAT Central Arizona Transmission EHV, SWAT Central Arizona HV, SWAT Colorado River Transmission, SWAT Arizona-New Mexico, and Southeast Arizona Transmission System (SATS). Each of these subcommittees has been involved in studying various generation and transmission projects to enhance and increase utilization of the existing system. The SATS study includes all or part of Pima, Pinal, Cochise, and Santa Cruz counties and has the largest direct impact on TEP.

TEP is a participant in the Hassayampa – Pinal West 500 kV project, which will be in service in 2008. TEP's Westwing – South 345 kV line will loop in at the new Pinal West 500/345 kV substation.

TEP is a participant in the Pinal West – Pinal South portion of the Pinal West – Southeast Valley 500 kV project. TEP plans to construct a 500 kV line between the proposed Pinal South Switchyard and TEP's Tortolita Substation in the year 2011.

TEP is evaluating various EHV alternatives for load serving capability within TEP's service territory including a possible 345 kV line between TEP's Tortolita Substation and Vail Substation with a loop in at the North Loop and East Loop Substations. Other alternatives are also being considered that will involve additional HV transmission within TEP's service territory.

01/28/2008

- 3 -

138kV Local Transmission System

TEP performs an annual review of its 138kV system performance over a ten-year planning horizon. This results in a schedule for new facilities and upgrades to existing facilities assuring adequate transmission capacity within TEP's service territory as Tucson continues to grow. TEP's 138kV system is improved to accommodate new 138/13.8kV substations, increased line loading, and mitigate localized stability issues.

Load projection analysis looks at distribution system needs and identifies the impact of load growth at each of TEP's distribution substations. This results in proposed new 138/13.8 kV substations and new 138kV transmission lines. Load projection also provides input to the power flow analysis used to identify thermal overloads as Tucson continues to grow.

Power flow analysis looks for thermal overloads during normal and contingency operation based on WECC/NERC Level A, B and C reliability criteria. Contingencies include:

- Loss of major EHV import
- Loss of critical local generation
- Single 138kV circuit outages
- Credible 138kV multiple circuit outages
- Critical circuits initially out of service with system operating acceptably followed by a subsequent outage.

Thermal overloads are addressed with:

- New transmission lines
- Uprating existing lines (increase NESC clearances or larger ampacity wire)
- New generation (when more economical than transmission)
- Other cost effective measures

Transmission facilities are also added at 138kV to increase reliability at substations that are served radially.

TEP is in the process of installing a -75 to +200 MVAr Static Var Ccompensator at its Northeast 138 kV substation scheduled to be in-service by the summer of 2008.





- 7 -

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Interconnection of Westwing – South 345 kV with future Hassyampa – Pinal West 500 kV lineⁱ via new Pinal West 500/345 kV Substation

Size

	a) Voltage	345-kV
	b) Capacity	System dependent
	c) Point of Origin	Westwing – South Line
	d) Point of Termination	Future Pinal West substation (Sec. 6 T5S R1E)
	e) Length	Less than 1 mile
Routir	ng	Adjacent to Westwing - South 345 kV line.
Purpo	se	To reinforce TEP's EHV system and to provide a higher capacity link for the flow of power from the Palo Verde area into TEP's service territory.
Date		
	a) Construction Start	2007
	b) In-Service Date	2008
Is Cer	tificate Necessary	Case #124
Techn	ical Studies	Studies completed via CATS, WATS, and Palo Verde – Southeast Station study groups.

'A joint project being jointly developed with SRP as project manager

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Pinal South Substation to Tortolita Substation

Size

a) Voltage	500-kV
b) Capacity	System dependent
c) Point of Origin	Future Pinal South substation
d) Point of Termination	Tortolita Substation (Sec. 14 T10S R10E)
e) Length	Approximately 30 miles
Routing	Unknown
Purpose	To reinforce TEP's EHV system and to provide a higher capacity link for the flow of power from the Palo Verde area into TEP's northern service territory.
Date	
a) Construction Start	2010
b) In-Service Date	2011
Is Certificate Necessary	Yes
Technical Studies	Studies in progress via SWAT and internal TEP study efforts.

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Tortolita Substation to Vail Substation (through North Loop and East Loop Substations)

Size

Date

	a) Voltage	345-kV
	b) Capacity	System dependent
	c) Point of Origin	Tortolita Substation (Sec. 14 T10S R10E)
	d) Point of Termination	Vail Substation (Sec. 4 T16S R15E)
	e) Length	Approximately 60 miles
Routin	ng	Unknown
Purpo	ose	To reinforce TEP's EHV system and to provide a new tie between TEP's HV and EHV systems.
D (

a) Construction Start	2013	
b) In-Service Date	Phase 1 – 2014	Tortolita Substation to North Loop Substation
	Phase 2 – Under Review	North Loop Substation to East Loop Substation
	Phase 3 – Under Review	East Loop Substation to Vail Substation
Is Certificate Necessary	Yes	
Technical Studies	Studies in progress v study efforts.	ia SWAT and internal TEP

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation		Tortolita Substation to Winchester Substation	
Size			
	a) Voltage	500-kV	
	b) Capacity	System dependent	
	c) Point of Origin	Tortolita Substation (Sec. 14 T10S R10E)	
	d) Point of Termination	Winchester Substation	
	e) Length	Approximately 80 miles	
Rout	ing	As described in Siting Case No. 23	
Purp	ose	To reinforce TEP's EHV system and to provide a higher capacity link for the flow of power from the Palo Verde area into TEP's eastern transmission system.	
Date			
	a) Construction Start	Under Review	
	b) In-Service Date	Under Review	
Is Ce	rtificate Necessary	Case No. 23	
Tech	nical Studies	Studies in progress via SWAT and internal TEP study efforts.	

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Winchester Substation to Vail Substation – 2^{nd} circuit

Size

a) Voltage 345-kV System dependent b) Capacity Winchester Substation c) Point of Origin Vail Substation (Sec. 4 T16S R15E) d) Point of Termination Approximately 40 miles e) Length Parallel to existing Winchester - Vail Line Routing To reinforce TEP's EHV system and to provide Purpose additional transmission capacity from the future Winchester Station into Tucson Date Under Review a) Construction Start b) In-Service Date **Under Review** Yes Is Certificate Necessary **Technical Studies**

Studies in progress via SWAT and internal TEP study efforts.

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Vail Substation to South Substation - 2nd circuit

Size

	a) Voltage	345-kV
	b) Capacity	System dependent
	c) Point of Origin	Vail Substation (Sec. 4 T16S R15E)
	d) Point of Termination	South Substation (Sec. 36 T16S R13E)
	e) Length	14 miles
Routin	ng	Parallel to existing Vail - South Line
Purpo	se	To reinforce TEP's EHV system and to provide additional transmission capacity between Vail and South Substations
Date		
	a) Construction Start	Under Review
	b) In-Service Date	Under Review
Is Cer	tificate Necessary	No
Techn	ical Studies	Studies in progress via SWAT and internal TEP study efforts.

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Springerville Substation to Greenlee Substation - 2nd circuit

Size

a) Voltage

b) Capacity

c) Point of Origin

d) Point of Termination

e) Length

Routing

Purpose

Date

a) Construction Start

b) In-Service Date

Is Certificate Necessary

Technical Studies

345-kV

System dependent

Springerville Substation (Sec. 34 T11N R30E)

Greenlee Substation (Sec. 29 T5S R31E)

110 Miles total; 27 Miles in Arizona.

Parallel to existing Springerville to Greenlee line.

To deliver power and energy from major TEP interconnections in the Four Corners and Eastern Arizona regions.

Under Review

Under Review

Issued in 1975, 1977, 1982 and 1986

Studies conducted in coordination with neighboring utilities formed the basis for the design of TEP's original EHV system in the 70's. This project is based on that original work. Detailed studies will be developed in the future upon a determination of need for this project by TEP.

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Tortolita Substation to South Substation.

Size

a) Voltage	345-kV
b) Capacity	System dependent
c) Point of Origin	Tortolita Substation (Sec. 23 T10S R10E)
d) Point of Termination	South Substation (Sec. 36 T16S R13E)
e) Length	68 Miles
Routing	From Tortolita Substation south through Avra Valley to existing Westwing-South 345-kV transmission line right-of-way, then parallel to existing Westwing – South line to South Substation.
Purpose	To reinforce TEP's EHV system and to provide a high capacity link for the flow of power in Southern Arizona.
Date	
a) Construction Start	Under Review
b) In-Service Date	Under Review
Is Certificate Necessary	Case #50
Technical Studies	Being re-evaluated as part of SWAT study

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

We stwing Substation to South Substation – $2^{\rm nd}$ circuit

Size

	a) Voltage	345-kV
	b) Capacity	System dependent
	c) Point of Origin	Westwing Substation (Sec. 12 T4N R1W)
	d) Point of Termination	South Substation (Sec. 36 T16S R13E)
	e) Length	178 Miles
Routin	ng	Parallel to existing Westwing to South line.
Purpo	se .	To deliver power and energy from major TEP interconnections in the Northwest Phoenix region.

Date

a) Construction Start	Under Review
b) In-Service Date	Under Review
Is Certificate Necessary	Case # 15
Technical Studies	Studies conducted in coordination with neighboring utilities formed the basis for the design of TEP's original EHV system in the 70's.

design of TEP's original EHV system in the 70's. This project is based on that original work. Detailed studies will be developed in the future upon a determination of need for this project by TEP.

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

TEP-Unisource Energy Services 345 kV Interconnection Line--South Substation to future Gateway Substation (2 ckts.)

Size

	a) Voltage	345-kV
	b) Capacity	500 MW
	c) Point of Origin	South Substation (Sec. 36 T16S R13E)
	d) Points of Termination	Gateway Substation in (Sec. 12 T24S R13E)
	e) Length	Approximately 60 Miles
Routii	ng	Southerly from South Substation, near Sahuarita Arizona to Nogales area.
Purpo	se	To provide an alternate transmission path to UNS Electric in Nogales, Arizona pursuant to ACC Order.
Date		
	a) Construction Start	Dependent upon permitting
	b) In-Service Date	Dependent upon permitting
Is Cer	tificate Necessary	Case #111
Techr	iical Studies	See record of Siting Case No. 111

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Size

Gateway Substation to Comision Federal de Electricidad (CFE) (2 ckts.)

	a) Voltage	345-kV
	b) Capacity	500 MW
	c) Point of Origin	Gateway Substation (Sec. 12 T24S R13E)
	d) Points of Termination	Arizona-Sonora boundary (Sec. 13 T24S R13E)
	e) Length	Approximately 2 Miles
Routir	ng	Southerly from Gateway Substation, in or near the Nogales area.
Purpo	se	To interconnect to the Comision Federal de Electricidad in Sonora, Mexico.
Date		
	a) Construction Start	Dependent upon permitting
	b) In-Service Date	Dependent upon permitting
Is Cer	tificate Necessary	Case #111
Techn	ical Studies	See record of Siting Case No. 111

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Irvington Substation to East Loop Substation (through 22nd Street Substation).

Size

a) Voltage	138-kV
b) Capacity	System dependent
c) Point of Origin	Irvington Substation (Sec. 03 T15S R14E)
d) Point of Termination	East Loop Substation (Sec. 08 T14S R15E)
e) Length	9 Miles
Routing	North and East of Irvington Substation, through 22nd Street Substation, then East and North to East Loop Substation.
Purpose	To provide additional electric service to the central area of TEP's service area and to reinforce the local transmission system.
Date	
a) Construction Start	1985

b) In-Service Date

Is Certificate Necessary

Phase 1 – 1994 (Completed)

Irvington Station to 22nd St. Substation

Phase 2 - 2000 (Completed)

22nd St. to East Loop Substation

2nd Circuit of Phase I

Phase 3 – Under Review

Case #66

10 YEAR PLAN

TRANSMISSION FACILITIES

Vail Substation to East Loop Substation (through Line Designation Houghton Loop Switching Station*, Spanish Trail and Roberts Substations), tapping the Roberts-East Loop line for new Harrison substation. Size 138-kV a) Voltage System dependent b) Capacity Vail Substation (Sec. 4 T16S R15E) c) Point of Origin East Loop Substation (Sec. 8 T14S R15E) d) Point of Termination 22 Miles e) Length East and north from Vail Substation along existing Routing transmission line to Irvington and Houghton Roads, then north along Houghton Road to Speedway Boulevard, then east and north to Roberts Substation and west along Speedway to East Loop Substation. To provide additional electric Purpose service to the eastern portion of TEP's service area and to reinforce the local transmission system. Date 1976 a) Construction Start Phase 1 - 1977 b) In-Service Date Spanish Trail (Completed) Substation to East Loop and Vail Substation Phase 2 - 1983 **Roberts Substation** and associated 138-kV lines (Completed) Phase 3 -**Under Review** Third 138-kV line from Vail to East Loop Substation Phase 4 -Harrison Substation tap of

Is Certificate Necessary

Case #8

*Houghton Loop switching station has been removed from TEP's plans. Name retained for reference

only.

Roberts-East Loop 138 kV

line

10 YEAR PLAN

TRANSMISSION FACILITIES

East Loop Substation to Northeast Substation Line Designation (through Snyder Substation) Size 138-kV a) Voltage System dependent b) Capacity East Loop Substation Sec. (8 T14S R15E) c) Point of Origin Northeast Substation Sec. (28 T13S R14E) d) Point of Termination 13 Miles e) Length North and west of East Loop Substation, then south Routing and west to termination point. To provide additional electric service to the Purpose northeastern area of TEP's service area. Date 1985 a) Construction Start Phase 1 - 1987 Snyder Substation and b) In-Service Date (Completed) 138-kV line to East Loop Substation 138-kV line from Phase 2 -1999-2005 Snyder Substation to Northeast Substation Interim line in service. Final completion date dependent on Pima County completion of public improvement project along Sunrise Dr. Pima County has not set a date for completion of this work.

Is Certificate Necessary

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Case #47

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Loop existing West Ina Substation to Tucson Station line through Del Cerro (formerly Sweetwater) Substation.

Size

a) Voltage	138-kV
b) Capacity	System dependent
c) Point of Origin	Sec. 20 T13S R13E
d) Point of Termination	Sec. 20 T13S R13E
e) Length	Less than one mile
Routing	Loop existing line at Camino del Cerro and Santa Cruz River; east along Camino del Cerro alignment into future Del Cerro Substation. Sec. 17 T13S R13E
Purpose	To provide additional electric service to the western part of TEP's service area and to reinforce the local distribution system.
Date	
a) Construction Start	2007
b) In-Service Date	2008
Is Certificate Necessary	Case #62

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Loop existing Vail Substation to East Loop Substation line through future Pantano and Los Reales Substations.

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a) Voltage b) Capacity

c) Point of Origin

-

d) Point of Termination

e) Length

Routing

Purpose

Date

a) Construction Start

b) In-Service Date

Is Certificate Necessary

138-kV

System dependent

Phase 1: Sec. 24, T15S R15E Phase 2: Sec. 28, T14S R15E Phase 1: Sec. 24, T15S R15E Phase 2: Sec. 28, T14S R15E

Substations are less than one span from the existing line.

Phase 1 Loop existing line east of Houghton Road and south of Valencia Road through Los Reales Substation.

Phase 2 Loop existing line east of Pantano Road and south of Golf Links through Pantano Substation.

To provide additional electric service to the eastern part of TEP's service area and to reinforce the local distribution system.

Phase 1 – 2001 Phase 2 - 2006

Phase 1 – Completed Phase 2 Completed

No

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Extend 138-kV line from Midvale Substation through future Spencer Switchyard to future San Joaquin Substation.

Size

a) Voltage

b) Capacity

c) Point of Origin

d) Point of Termination

e) Length

Routing

Purpose

Date

a) Construction Start

b) In-Service Date

Is Certificate Necessary

138-kV

System dependent

Midvale Substation (Sec. 3 T15S R13E)

Future San Joaquin Substation (physical location to be determined)

Approximately 20 miles

Reviewing use of common utility corridor and existing subtransmission

To provide additional electrical service to the far western portion of TEP's service area and to reinforce the local distribution system.

2012

2013

Under Review (dependent upon use of federal and/or Tohono r/w)

10 YEAR PLAN

TRANSMISSION FACILITIES

South Substation to Duval CLEAR Switchyard Line Designation (formerly Cyprus Sierrita Extension Switchyard) through future Canoa Ranch (formerly Desert Hills) Substation and Green Valley Substation Size 138-kV a) Voltage System dependent b) Capacity c) Point of Origin South Substation (Sec. 36 T16S R13E) Duval CLEAR Switchyard (formerly Cyprusd) Point of Termination Sierrita Extension Switchyard) (Sec. 10 T18S R12E) e) Length Approximately 24 miles Routing Uses existing transmission, sub-transmission, and overhead distribution route. To provide additional electrical service to southern Purpose area of TEP's service area and to reinforce the local transmission & distribution system. Date 1995 a) Construction Start Phase 1 -1997 South 138-kV b) In-Service Date line to Green Valley. (Completed) Phase 2a -2006 138-kV line from Green (Completed) Valley to future Canoa Ranch Substation site Phase 2b- 2013 Extend 138-kV line from Canoa Ranch Substation site to future Duval CLEAR Switchyard (formerly Cyprus Sierrita Extension

Is Certificate Necessary

(Extension approved in 2006 ACC Order # 69680, docketed 6/28/07)

Switchyard)

Case 84

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Size

Rancho Vistoso Substation to future Catalina Substation

a) Voltage	138-kV
b) Capacity	System dependent
c) Point of Origin	Rancho Vistoso Substation (Sec. 36 T11S R13E)
d) Point of Termination	Future Catalina Substation Sec. 18 T11S R14E
e) Length	Approximately 3.5 Miles
Routing	Existing Western Area Power Administration corridor
Purpose	To provide additional electrical service to far northern area of TEP's service area and to reinforce the local distribution system.
Date	
a) Construction Start	2009
b) In-Service Date	2010
Is Certificate Necessary	No

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation Loop existing Irvington Station to Vail Substation #2 line through future University of Arizona Tech Park Substation.

Size

a) V	/oltage	138-kV
b) (Capacity	System dependent
c) P	oint of Origin	Vail – Irvington Corridor
d) I	Point of Termination	Future U of A Tech Park Substation approximately Sec. 28 T15S R15E
e) L	Length	Approximately 5 miles of double-circuited line
Routing		Loop existing Irvington – Vail #2 line into future U of A Tech Park substation
Purpose		To provide additional electric service to the U of A Tech Park expansion and the southern part of TEP's service area.
Date		
a) (Construction Start	2012
b) I	n-Service Date	2013
Is Certifica	te Necessary	Yes

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Tortolita Substation - Rillito Substation 138 kV

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51	70
\mathbf{u}	20

	a) Voltage	138-kV
	b) Capacity	System dependent
	c) Point of Origin	Tortolita 138 kV Substation
	d) Point of Termination	Rillito 138 kV Substation
	e) Length	24.5 miles
Routin	ng	Unknown
Purpose		Required to fully utilize increased import capability of additional EHV capacity into Tortolita Substation (Pinal South – Tortolita).
Date		
		1

a) Construction Start	Under review
b) In-Service Date	Under review
Is Certificate Necessary	Yes

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Tortolita Substation – North Loop Substation, North Loop Substation – Rancho Vistoso Substation and Tortolita – Rancho Vistoso 138 kV corridor expansion and reconfiguration

Size

along

a) Voltage

b) Capacity

c) Points of Origin

d) Points of Termination

e) Length

138-kV

System dependent

Tortolita 138 kV Substation North Loop 138 kV Substation

North Loop 138 kV Substation Rancho Vistoso 138 kV Substation

Tortolita – North Loop: ~14.3 miles North Loop – Rancho Vistoso: ~11.1 miles

f) Routing Phase 1: Re-configure Tortolita – Rancho Vistoso line as a third Tortolita - North Loop line utilizing existing 138 kV stub out of North Loop. Build new bay at North Loop to accommodate North Loop – Rancho Vistoso line utilizing existing 138 kV pole-line Tangerine Rd.

SWTC to construct a new fourexisting the

Tortolita-North Loop lines, a fourth and

Phase 2: A joint project with circuit pole-line to replace single-circuit structures on Tortolita-North Loop 138 kV corridor. The four-circuit structures will accommodate the two existing Tortolita – North Loop line SWTC's Saguaro – Camino de Manana 115 kV circuit.

Tortolita – North Loop line from

Phase 3: Re-route the third Phase 1 above to terminate at Rancho Vistoso; ~ 9.0 miles of Rancho Vistoso; ~ 9.0 miles of
along Tangerine Rd.
will be uprated to 138 kV. Tap theNorth Loop - Rancho Vistoso line to supply thenew Naranja 138/13.8 kV substation

2008

Purpose

Required for NERC N-1 issues on these parallel path circuits.

Date

f) Construction Start

g) In-Service Date

Phase 2: 2009 Phase 3: 2010

Phase 1: 2008

Is Certificate Necessary

Phase 1: Yes Phase 2: Yes

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Vail Substation – SS NO27 Substation- Cienega Substation – SS NO20 Substation- Spanish Trail Substation 138 kV

Size		
	a) Voltage	138-kV
	b) Capacity	System dependent
	c) Point of Origin	Vail 138 kV Substation
	d) Point of Termination	Spanish Trail 138 kV Substation
	e) Length	Phase 1: Vail - Cienega ~12.2miles Phase 2: Vail - SSNO27 ~5.3 miles Phase 3: Cienega - SS NO20 ~14.0 miles
Routing		Phase 1: Utilize the existing Vail-Fort Huachuca/ Vail- Spanish Trail 138 kV corridor between Vail Substation and seven spans east of Wentworth Rd., then new double-circuit 138 kV northeast ~2.0 miles to proposed Cienega site in T16S R16E Sec 16.
		Phase 2: Tap the Vail – Cienega 138 kV line from Phase 1 and extend new double-circuit 138kV ~ 2.0 miles south along Houghton Rd. to proposed SS NO27 substation site.
		Phase 3: Tap the Cienega – Spanish Trail line from Phase 1 and new circuit out of Los Reales extended via new triple- circuit 138kV east of Los Reales ~ 3.0 miles east along Los Reales Rd to proposed SS NO20 substation site ~ 0.75 miles east of E. Old Spanish Trail.
Purpo	ose	Required to serve load at the new Cienega 138/13.8 kV Substation located approximately 7.5 miles east-southeast of the Vail Substation, and the future SS NO27 and SS NO20 138/13.8 kV Substations located approximately 4.0 miles southwest and 6.0 miles north of the Cienega Substation, respectively.
Date		Phase 1: Cienega a) Construction Start 2008 b) In-Service Date 2010
		Phase 2: SS NO27 a) Construction Start 2018 b) In-Service Date 2020

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Phase 3: SS NO20a) Construction Start2021b) In-Service Date2023

Is Certificate Necessary

Yes

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Size

New Cienega Substation – Mountain View Substation 138 kV Circuit and Vail Substation – Fort Huachuca Tap for Mountain View Substation

a) Voltage	138-kV
b) Capacity	System dependent
c) Point of Origin	Cienega 138 kV Substation (T16S R16E Sec 16)
d) Point of Termination	Mountain View 138 kV Substation (T17S R16E Sec 2)
e) Length	4.7 miles
Routing	Extend 138 kV pole-line out of the Cienega substation east along Dawn Dr. to the Southern Pacific Railroad, then southeast along railroad, then south to the Mountain View Substation site.
	In addition the Mountain View substation will tap the existing Vail Substation – Ft. Huachuca Substation line to increase reliability to Mountain View with a modest improvement in voltage regulation to Ft. Huachuca.
Purpose	Required to serve load at the new Mountain View 138/13.8 kV Substation approximately 11 miles south-southeast of the Vail Substation
Date	
a) Construction Start	TBD
b) In-Service Date	TBD
Is Certificate Necessary	Yes

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Northeast – Snyder 138 kV – tap for Craycroft-Barril substation

Size

a) Voltage	138-kV
b) Capacity	System dependent
c) Point of Origin	Northeast 138 kV Substation
d) Point of Termination	Snyder 138 kV Substation
e) Length	8.0 miles
Routing	Existing Northeast-Snyder Corridor requires 1 span of wire to drop into station.
Purpose	Required to serve load at the new Craycroft-Barril 138/13.8 kV Substation locate approximately 2.75 miles northeast of the Northeast Substation
Date	
a) Construction Start	2010
b) In-Service Date	2011
Is Certificate Necessary	No

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Irvington – Tucson 138 kV – tap for Kino Substation

Size

a) Voltage	138-kV
b) Capacity	System dependent
c) Point of Origin	Irvington 138 kV Substation
d) Point of Termination	Tucson 138 kV Substation
e) Length	10.9 miles
Routing	Existing Irvington-Tucson Corridor And ~ 3.0 miles of new double-circuit corridor north of Drexel along Kino Parkway to 36 th St.
Purpose	Required to serve load at the new Kino 138/13.8 kV Substation located approximately 5.0 miles northwest of the Irvington Substation
Date	
a) Construction Start	2010
b) In-Service Date	2012
Is Certificate Necessary	Yes

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10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Tortolita Substation – Marana Substation – North Loop Substation 138 kV and Marana Substation – SS NO1 Substation -North Loop Substation 138 kV

Size

a) Voltage

b) Capacity

c) Point of Origin

d) Point of Termination

e) Length

Routing

Purpose

Date

Marana (Phase 1)

SS NO1 (Phase 2)

138-kV

System dependent

Phase 1: Tortolita 138 kV Substation Phase 2: Marana 138 kV Substation

North Loop 138 kV Substation

Phase 1: Tortolita – Marana ~11.0 miles Marana - North Loop ~11.0 miles

Phase2: Marana – SSNO1 ~6.0 miles SSNO1 – North Loop ~7.5 miles

Phase 1: Tap the Tortolita- North Loop corridor at the Trico-Marana Rd. alignment and extend ~ 4 miles of double-circuit pole-line west across I-10 to proposed Marana substation site near Sanders Rd.

Phase 2: approximately 13.5 miles of new corridor between Marana and Tortolita 138 kV substations located west of I-10

Phase 1:Required to serve load at the new Marana 138/13.8 kV Substation located approximately 9.0 miles south-southeast of the Tortolita Substation Phase 2: Required to serve load at the new SS NO1 138/13.8 kV Substation located approximately 6.0 miles south-southeast of the Marana Substation

a) Construction Start 2011b) In-Service Date 2013

a) Construction Start 2021

b) In-Service Date 2023

Is Certificate Necessary

Yes

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

North Loop Substation - Rancho Vistoso Substation 138kV tap for new Naranja Substation

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a) Voltage	138-kV
b) Capacity	System dependent
c) Point of Origin	North Loop 138 kV Substation
d) Point of Termination	Naranja 138 kV Substation
e) Length	North Loop – Naranja ~7.9 miles Naranja – Ranch Vistoso ~16.6 miles
Routing	Tap the North Loop – Rancho Vistoso line created as part of the Tortolita Substation – North Loop Substation and North Loop Substation – Rancho Vistoso Substation 138 kV corridor expansion and reconfiguration project. Extend ~ 3.0 miles of new double circuit corridor south of Tangergine Rd. along Thornydale Rd. to the substation site
Purpose	Required to serve load at the new Naranja 138/13.8 kV Substation located in the vicinity of Thornydale Rd. and Lambert Ln.
Date	
a) Construction Start	2009
b) In-Service Date	2010
Is Certificate Necessary	Yes

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

DeMoss Petrie Substation – Tucson Substation 138 kV

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a) Voltage	138-kV
b) Capacity	System dependent
c) Point of Origin	DeMoss Petrie 138 kV Substation
d) Point of Termination	Tucson 138 kV Substation
e) Length	4.5 miles
Routing	existing DeMoss Petrie - Tucson 46 kV corridor
Purpose	Required to eliminate localized voltage instability specific to loss of both the North Loop-West Ina and Irvington-Tucson 138 kV circuits. By 2010, the existing 46 kV tie between DMP and Tucson Stations is unable to support voltage of the Tucson and West Ina load during this contingency.
Date	
a) Construction Start	2009
b) In-Service Date	2010
Is Certificate Necessary	Yes

10 YEAR PLAN

TRANSMISSION FACILITIES

Element Designation	Northeast 138 kV Static Var Compensator (SVC)
Size	
a) Voltage	138-kV
b) Capacity	-75 to +200 MVAr
c) Location	Northeast 138 kV Substation
Purpose	The SVC is being installed to reduce, and in some cases eliminate, the need for direct load tripping required for stable operation during system contingencies. As a dynamic VAr source, the SVC also reduces the amount of generation that would otherwise have to run to provide these dynamic VArs
Date	
a) Construction Start	2007 - project underway
b) In-Service Date	2008
Is Certificate Necessary	No

Study work used to justify the SVC attached as Appendix A:

Voltage Stability Study of the Tucson Electric Power 138 kV System, 8/19/05

Voltage Stability Study of the Tucson Electric Power 138 kV System Phase II , 10/4/06

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

North Loop Substation – SS NO4 Substation – DeMoss Petrie Substation 138kV

138-kV a) Voltage System dependent b) Capacity North Loop 138 kV Substation c) Point of Origin **DeMoss Petrie Substation** d) Point of Termination North Loop – SS NO4 ~4.5 miles e) Length SS NO4 – DeMoss Petrie ~11.3 miles Tapping the existing North Loop - West Ina 138kV Routing circuit and extending approximately 2 miles of new double circuit pole-line southwest along Cortaro Farms Rd. to the substation site. Required to serve load at the new SS NO4 138/13.8 Purpose kV Substation Date 2028 a) Construction Start 2030 b) In-Service Date Yes Is Certificate Necessary

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Size

Midvale Substation – SS NO22 Substation – South Substation 138kV

a) Voltage	138-kV
b) Capacity	System dependent
c) Point of Origin	Midvale 138 kV Substation
d) Point of Termination	South 138kV Substation
e) Length	Midvale - SS NO22~6.0 milesSS NO22 - South~7.0 miles
Routing	Tapping the existing Midvale - South 138kV circuit
Purpose	Required to serve load at the new SS NO22
Date	138/13.8 kV Substation
a) Construction Start	2017
b) In-Service Date	2019
Is Certificate Necessary	Yes
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10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Size

Irvington Substation - Corona Substation -Swan Southlands Substation - SS NO26 Substation -South Substation 138kV

Size		
	a) Voltage	138-kV
	b) Capacity	System dependent
	c) Point of Origin	Irvington 138 kV Substation
	d) Point of Termination	South 138kV Substation
	e) Length	Phase 1: Irvington - Corona ~3.0 miles Corona - South ~13.1 miles
		Phase 2: Corona - SS NO26 ~7.0miles SS NO26 - South ~6.1 miles
		Phase 3: Corona – Swan Southlands ~13.1 miles Swan South – SS NO26 ~3.0 miles
Routin	e	Tapping the existing Irvington – South 138kV circuit.
Purpos	se	Phase 1: Required to serve load at the new Corona 138/13.8 kV Substation
		Phase 2: Required to serve load at the new SS NO26 138/13.8 kV Substation
Date		Phase 3: Required to serve load at the new Swan Southlands 138/13.8 kV Substation
		Phase 1: Coronaa) Construction Start2011b) In-Service Date2013
		Phase 2: SS NO26a) Construction Start2014b) In-Service Date2016

Phase 3: Swan Southlands

a) Construction Start 2016 b) In-Service Date 2018

Is Certificate Necessary

Yes

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

La Canada Substation – Orange Grove Substation– Rillito Substation 138kV

Size

a) Voltage	138-kV
b) Capacity	System dependent
c) Point of Origin	La Canada 138 kV Substation
d) Point of Termination	Rillito 138kV Substation
e) Length	La Canada - Orange Grove ~3.8 miles Orange Grove - Rillito ~1.6 miles
Routing	Tapping the existing La Canada - Rillito 138kV circuit and drop into new station adjacent to the right-of-way at La Canada Blvd. and Orange Grove Rd.
Purpose	Required to serve load at the new Orange Grove 138/13.8 kV Substation
Date	
a) Construction Start	2011
b) In-Service Date	2013
Is Certificate Necessary	Yes

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Orange Grove Substation-SS NO6 Substation 138kV

Size

a) Voltage	138-kV
b) Capacity	System dependent
c) Point of Origin	Orange Grove 138 kV Substation
d) Point of Termination	SS NO6 138kV Substation
e) Length	Orange Grove – SS NO6 ~3.6 miles
Routing	Radial 138kV circuit from Orange Grove to SS NO6
Purpose	Required to serve load at the new SS NO6 138/13.8 kV Substation
Date	KV Substation
a) Construction Start	2015
b) In-Service Date	2017
Is Certificate Necessary	Yes

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

South Substation – Hartt Substation– Green Valley Substation 138kV

Size	
a) Voltage	138-kV
b) Capacity	System dependent
c) Point of Origin	South 138 kV Substation
d) Point of Termination	Green Valley 138kV Substation
e) Length	South - Hartt ~11.0 miles Hartt - Green Valley ~3.5 miles
Routing	Tapping the existing South – Green Valley 138kV circuit and drop into new station adjacent to the right-of-way ~ 1 mile south of Old Nogales Hywy and Duval Mine Rd.
Purpose	Increase load serving and reliability of existing 46/13.8 facilities near this site.
Date	
a) Construction Start	2011
b) In-Service Date	2013
Is Certificate Necessary	Yes
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10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Hartt Substation-SS NO29 Substation 138kV

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a) Voltage	138-kV
b) Capacity	System dependent
c) Point of Origin	Hartt 138 kV Substation
d) Point of Termination	SS NO29 138kV Substation
e) Length	Hartt - SS NO29 ~7.1 miles
Routing	Radial 138kV circuit from Hartt to SS NO29
Purpose	Required to serve load at the new SS NO29
Date	158/15.8 KV Substation
a) Construction Start	2014
b) In-Service Date	2016
Is Certificate Necessary	Yes

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Tucson Substation- Downtown Substation 138kV

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a) Voltage	138-kV
b) Capacity	System dependent
c) Point of Origin	Tucson 138 kV Substation
d) Point of Termination	Downtown 138kV Substation
e) Length	Tucson – Downtown ~1.0 mile
Routing	Radial 138kV circuit from Tucson to Downtown
Purpose	Required to serve load at the new Downtown
Date	156/ 15.6 KV Substation
a) Construction Start	2010
b) In-Service Date	2012
Is Certificate Necessary	Yes

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

DeMoss Petrie Substation-SS NO14 Substation -Northeast Substation 138kV

Size

a) Voltage

b) Capacity

c) Point of Origin

d) Point of Termination

e) Length

Routing

Purpose

138-kV

System dependent

DeMoss Petrie 138 kV Substation

Northeast 138kV Substation

DeMoss Petrie - SS NO14 ~7.5 miles SS NO14 - Northeast ~6.0 miles

New 138kV Construction between DeMoss Petrie and Northeast 138kV substations. SS NO14 is approximately located south-southeast of Northeast Substation.

Required to serve load at the new SS NO14 138/13.8 kV Substation

Date 2024 a) Construction Start 2026 b) In-Service Date Yes Is Certificate Necessary

10 YEAR PLAN

TRANSMISSION FACILITIES

Line Designation

Vail Substation - SS NO17 Substation - Irvington Substation 138kV

Size			
a) Voltage	138-kV		
b) Capacity	System dependent		
c) Point of Origin	Vail 138 kV Substation		
d) Point of Termination	Irvington 138kV Substation		
e) Length	Vail - SS NO17~6.5 milesSS NO17 - Irvington~3.5 miles		
Routing	New 138kV Construction between Vail and Irvington 138kV substations. SS NO17 is located ~2.5 miles north of Robert Bills 138kV substation.		
Purpose Date	Required to serve load at the new SS NO14 138/13.8 kV Substation		
a) Construction Start	2018		
b) In-Service Date	2020		
Is Certificate Necessary	Yes		

Appendix A

Static VAr Compensator Voltage Stability Studies

Electric Systems Consulting

Technical Report

ABB inc.			
Title: Voltage Stability Study of the Tucson	Dept.	Date	Pages
Electric Power 138 kV System: Final Report	Consulting	8/19/2005	83

Author(s):

Reviewed/Approved by:

Pouyan Pourbeik

Willie Wong

Executive Summary:

This report describes the results and recommendations of the voltage stability study performed of the Tucson Electric Power (TEP) 138 kV transmission network.

The scenarios studied are for peak load conditions between 2006 to 2010. In addition, some sensitivity analysis was performed for a peak 2015 planning horizon case. *The intent of this study was to focus only on a minimum local generation scenario.* A minimum TEP generation scenario was studied in which all the local generation with the exception of the large steam unit at Irvington power station (Sundt #4) was taken out of service.

Based on both steady-state and time-domain analysis, the following reactive compensation additions are required to ensure stable and reliable system operation under the minimum local TEP generation scenarios, for all possible category B and C outages on the 138 kV network and select critical 345 and 500 kV lines surrounding the TEP area:

- To increase all existing shunt capacitor banks to their maximum size through the addition of extra capacitor cans, by 2006. This means increasing the size of the capacitors at Northeast, Rillito, Tucson and Westina to 50.8 MVAr each, those at South to 50.9 MVAr each and the Northeast RAS capacitor to 52 MVAr.
- To install a +200/-75 MVAr SVC at Northeast 138 kV substation that is coordinated with all of the mechanically switched capacitor banks at that substation. As such, the existing RAS capacitor at Northeast would be switched by the SVC automatically and thus removed from RAS action.
- To incrementally add the following shunt capacitor banks from 2006 to 2015:
 - A 50.8 MVAr capacitor at Northeast in 2006.
 - A 25.4 MVAr capacitor at Roberts, and a 50.8 MVAr capacitor at North Loop and Irvington in 2009.
 - o To increase the size of the Roberts 25.4 MVAr capacitor to 38.1 MVAr in 2015.

Based on a time frame of 2006 to 2010, the SVC size need only be $\pm 150/-75$ MVAr. To extend the period to 2015, the SVC size should be increased to $\pm 200/-75$ MVAr. Thus the largest SVC size has been quoted above to cover all the cases studied. This is because it is likely more economical to install a $\pm 200/-75$ MVAr SVC to begin with rather than to attempt to add to the device in future years, or to install a smaller device first and then a second SVC. Thus, if it is the intend of TEP to be able to maintain a minimum generation scenario up to and including 2015 during peak load times, the recommended solution is a $\pm 200/-75$ MVAr SVC with gradual addition of the proposed shunt capacitor banks as described above.

The above recommendations are supported by both the results of the steady-state and time-domain simulations. It is shown in the report that in order to maintain reliable system operation under various credible load modeling assumptions, the most robust solution option (with a focus on sizing the dynamic device in order to avoid exorbitant cost) is that provided above. These reactive additions are required to ensure stable system response to all category B outages on the 138 kV and surrounding EHV (345 and 500 kV) lines and transformers. For category C and higher, Remedial Action Scheme (RAS) load shedding is also required.

Both steady-state and time-domain simulations were performed to confirmed that RAS load shedding will be necessary for a number of category C outages. Power flow analysis was performed to confirm that all of the category C outages can be solved by either the proposed additional shunt compensation or the combined

application of this shunt compensation together with an appropriate amount of RAS load shedding and the application of the RAS reactor at South. Although the RAS capacitors at Vail were not used, this is not necessarily an indication that they are not needed for category C and D outages. Here the purpose of the N-2 contingency analysis was simply to illustrate that a solution can be achieved with the combination of RAS (load shedding and reactive devices) and the added reactive compensation. Therefore, we simply found a way to achieve a solution in each case. A more optimal solution may exist with the application of the RAS capacitors. The optimization of the RAS load shedding and reactive devices, for category C and D outages, is outside the scope of this study. Time-domain simulations were also performed for the most onerous category C cases to illustrate that the combination of the additional shunt compensation and RAS load shedding can indeed achieve a stable system response.

Through the N-2 contingency analysis a couple of double contingencies were identified that may warrant further investigation. One of these results in problems in the New Mexico system and the other results in severe voltage depressions in Zone 161. Since both areas are outside the study area being investigated here, no further action was taken for the purposes of this study.

Finally, it should be emphasized again that the above reactive additions are recommended for the purpose of allowing reliable system operation during peak load hours under a TEP minimum local generation scenario. Recently discussions with TEP (since late June, 2005) have identified that the propose minimum generation scenario may not be realizable as early as 2006 due to thermal and other system operating constraints. Thus, reaching the minimum generation scenario may be a more gradual process as other issues are addressed in parallel. As such, the need for the SVC (and possibly its size) as well as the exact timing of phasing in the additional shunt capacitor additions will be impacted by the actual generation dispatch scenarios to be considered. Such determinations require further analysis, and are beyond the scope of this report.

Electric Systems Consulting

Technical Report

ABB Inc.			
Title: Voltage Stability Study of the Tucson	Dept.	Date	Pages
Electric Power 138 kV System – Phase II: Final Report	Consulting	10/4/2006	76

Author(s):

Reviewed/Approved by:

Willie Wong

Pouyan Pourbeik

Executive Summary:

This report describes the results and recommendations of the Phase II voltage stability study performed of the Tucson Electric Power (TEP) 138 kV transmission network.

In 2005, a comprehensive analysis was performed of the TEP system looking at a single generation dispatch scenario – minimum local generation (only Sundt #4 on-line). For this analysis, summer peak load cases were studied for 2006 to 2010. In addition, some sensitivity analysis was performed for a peak 2015 planning horizon case.

Based on detailed steady-state analysis (contingency analysis, PV, QV and OPF) and time-domain analysis, it was found that voltage stability concerns did exist within the TEP system for this minimum generation scenario and that the most robust solution, which would cover all cases through 2015, is a smoothly controlled dynamic reactive device. That is, a $\pm 200/-75$ MVAr SVC located at Northeast substation and coordinated with four 50 MVAr capacitor banks at the same substation (these shunt banks would be essentially the existing three shunt capacitor). Also, some additional mechanically switched capacitors were recommended at other substations for the purpose of ensuring adequate steady-state voltage profile and stability.

This report describes the time-domain, and some limited steady-state analysis, associated with Phase II of this study. After completion of the Phase I work in 2005, TEP proceeded to perform an extensive and comprehensive analysis of the system focusing on thermal and voltage criteria from a steady-state perspective. All N-1 and N-2 (essentially N-1-1) cases were investigated. Based on this analysis required minimum local generation scenarios (RLG) were established as well as transmission augmentation and discreet shunt compensation additions in order to address thermal and voltage criteria violations. Also, both SVC and non-SVC cases were investigated. In general, the results of the steady-state contingency analysis (performed by TEP) may be briefly summarized as follows:

- For the RLG cases established with the SVC in-service the only non-convergent power flow solutions were a few N-1-1 outages that involved the loss of the SVC as one of the outages¹. This is clearly no surprise, since the SVC was established to ensure voltage stability.
- For the RLG cases without the SVC many N-1-1 cases result in divergent power flows, which is
 indicative of voltage stability concerns.
- The RLG in general tends to be less with the SVC in-service thus establishing an additional economic benefit of requiring less of the expensive local generation to be on-line for the purpose of serving load.

Based on these results, the decision has been made to move forward with the SVC option. However, to ensure that the steady-state results are indicative of the expected dynamic performance of the system some further time-domain simulations was needed; that is the purpose of this report and study.

In this study, the RLG cases established by TEP's steady-state analysis were used as a starting point. Then the

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¹ Two other outages also resulted in non-convergent power flows. The loss of the Irvington ~ Tucson 138 kV and North Loop – West Ina 138 kV and the loss of Hidalgo – P Young 345 kV and Springerville – Luna 345 kV. As shown in previous work (such as the Phase I study) the former of these outages results in radially back-feeding a pocket of load off of the 46 kV network and the latter is related to problems in a neighboring system. Thus, these two outages were not further investigated in this study.

worst N-1 and N-1-1 outages were identified through steady-state analysis. These critical outages were then simulated in time-domain. The results of this time domain analysis confirms that:

- 1. The SVC is needed to ensure stability and provided for greater voltage regulation and a faster voltage recovery post-disturbance.
- The proposed location and size of the SVC is adequate through 2015; that is, at the Northeast 138 kV substation, coordinated with the MSCs at that substation and having a rating of +200/-75 MVAr (as seen at the 138 kV level).
- 3. The additional proposed shunt capacitor banks (mechanically switched) as included in the TEP RLG cases for the study years is needed for steady-state voltage support.

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